

## SIZE DISTRIBUTION OF DROPLETS OF A DISPERSED PHASE AT FERMENTATION

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The size distribution of droplets for a series of batch fermentation experiments was studied by taking photographs of samples of hydrocarbon emulsion stabilized in a gelatine media in a laboratory size and at pilot-plant conditions. The time dependence, dependence on volume fraction of hydrocarbons and on the size of inocula at fermentation of hydrocarbons by use of *Candida lipolytica* 4-1 yeasts were studied. The suitability of Pearson's functions for description of the obtained distributions and the data in the literature which were characterized by a strong right asymmetry, was verified.

This contribution is related to a recent study<sup>1</sup> in which some momentum characteristics of size distribution of droplets in an emulsion of gas oil and n-hexadecane dissolved in a deparafined gas oil were studied. An attempt is made here to describe the size distribution of droplets by use of a suitable mathematical relation which would make possible a more accurate modelling of the fermentation kinetics in an aerated batch with two liquid phases: medium-hydrocarbon.

The present state of knowledge on modelling of fermentation operations in the considered system is given *e.g.* by Shah and coworkers<sup>2</sup>. Erickson and coworkers<sup>3</sup> applied for the kinetics the rectangular size distribution of droplets as the first approximation; then the distribution according to Chen and Middleman<sup>4</sup>

$$f_v(x/\bar{x}_{32}) = (s_v\sqrt{2\pi})^{-1} \exp [(x - \bar{x}_v)^2/2s_v^2], \quad (1)$$

where  $\bar{x}_{32}$  is the Sauter's mean,  $\bar{x}_v$  and  $s_v^2$  is the average and the estimate of variance of the volume distribution, and  $f_v(x/\bar{x}_{32})$  is the volume weighted frequency function.

Katinger<sup>5</sup> has made an attempt to describe the size distribution of droplets in the considered system by use of the relation published by Schwarz and Bezemer<sup>6</sup>

$$f_v(x) = a/x^2 \cdot \exp(a/X - a/x), \quad (2)$$

where  $a$  and  $X$  are empirical parameters, which can be determined from the linear regression relation

$$\ln [v(x)] = k_1 - k_2(1/x). \quad (3)$$

According to relation (3)  $v(x)$  represents the cumulative volume fractions in %, and  $x$  is the size of droplets. The parameters of function (2) are related with the constants of regression (3) by the following equations

$$a = k_2, \quad (4)$$

$$X = a[k_1 - \ln 100]^{-1}. \quad (5)$$

Schwarz and Bezemer<sup>6</sup> are also giving the relation for the frequency function of droplet sizes

$$f(x) = \exp(a/X) / [6(1 + a/X + a^2/2X^2 + a^3/6X^3)] a^4/x^5 \cdot \exp(-a/x). \quad (6)$$

Experimentally determined distributions of droplet sizes of hydrocarbons at fermentation have been published only by few authors — like Katinger and coworkers<sup>7,8</sup> and Wang and Ochoa<sup>9</sup>. McLee and Davies<sup>10</sup> have published distributions concerning emulsions obtained in laboratory separating funnels and thus they are not of interest for this study. Rajagopal<sup>11</sup> has applied for description of size distribution of droplets in an oil emulsion the log-normal distribution which is in general suitable for distributions with the right asymmetry. As long as the transformation

$$x = 1/c \exp(cs), \quad (7)$$

is used where  $c = 1/M$  (where  $M$  is median) and  $s$  is the standard deviation for the variable of the normalized Gaussian distribution, then for the log-normal frequency function is obtained the relation given by Gebelein<sup>12</sup>

$$f(x) = \lambda^{1/2} [s(2\pi)^{1/2}]^{-1} \exp[-(z + cs)^2/2], \quad (8)$$

$$\lambda = \exp(c^2 \cdot s^2) \quad (9)$$

and  $z$  is the inverse transformation to Eq. (7). Steidl<sup>13</sup> has derived for the turbulent emulsion the relation for stationary distribution of drop sizes, the validity of which was verified<sup>14</sup> in a series of experiments with mechanical mixers for coarse emulsions with drop sizes above 50  $\mu\text{m}$ .

#### Expression for Distribution of Drop Sizes in Emulsion

Together with the frequency function  $f(x)$  defined *e.g.* by relation

$$dn = f(x) dx, \quad (10)$$

where  $dn$  is the number of drops with dimensions satisfying condition  $x \in (x, x + dx)$ , the so-called weighted frequency functions are also frequently used giving the distribution of volumes or surface areas of particles. In this case *e.g.* the volume weighted frequency function  $f_v(x)$  is defined by

$$dv = f_v(x) dx = k_v x^3 dn. \quad (11)$$

In Eq. (11)  $k_v$  is the shape factor for volume of particles (for spherical drops in an emulsion it can be accepted  $k_v = \pi/6$ ). Recalculation of frequencies from the volume weighted frequency function (without considering the functional transformation) is affected by a great error. If  $\Delta n$  is the absolute error of frequencies corresponding to a finite interval of size  $\Delta x$  (which is a quantity

proportional to the relative error of the frequency function (10)), from relations (10) and (11) results

$$\Delta n/\Delta x \approx dn/dx = f(x) = f_v(x) (k_v x^3)^{-1}. \quad (12)$$

For illustration are in Fig. 1 given, for one typical experiment, the ranges limited by 10% error of the frequency function  $f(x)$  — the region limited by solid lines (error at direct determination of frequencies). Dashed lines are limiting the region of fluctuating frequencies at their recalculation from the volume function  $f_v(x)$  which is affected by the same relative deviation of 10%. It is obvious that frequencies of fine particles which are of great importance in fermentation cannot be reliably determined at all from the course of the function  $f_v(x)$ . For this reason we have not studied the suitability of the volume distribution according to Chen and Middlemann (Eq. (1)).

#### Verification of Relations Published for Frequency Functions

Analysis of suitability of frequency functions for drop sizes which had been derived on basis of physical models of formation of an emulsion and the review of which is *e.g.* given by Shah and coworkers<sup>2</sup> or by Steidl and Ludvík<sup>13,14</sup> was negative. These functions include<sup>2</sup> a great number of parameters of emulsion which can be determined with a great difficulty or which are not suitable due to their shape. Also the log-normal distribution which is based on a quite general model of particle desintegration is not satisfactory for our experimental data. On basis of the relation for the moments about origin of log-normal distribution as given by Gebelein<sup>12</sup>

$$\mu_r(x) = c^{-r} \lambda^{r^2/2}, \quad (13)$$

can be derived relations for the coefficient of asymmetry  $S_k$

$$S_k = m_3 s^{-3} = (\lambda + 2)(\lambda - 1)^{0.5}, \quad (14)$$

where  $m_3$  is the central moment of the third order and  $s$  is the standard deviation. For the coefficient of excess  $E_k$  then results

$$E_k = (m_4 s^{-4}) - 3 = [\lambda^6 - 4\lambda^3 + 6\lambda^{3/2}c^{-1} - 3] / [c^{-4}\lambda^2(\lambda^4 - 4\lambda^3 + 6\lambda^2 - 5\lambda + 1)] - 3. \quad (15)$$

Comparison of coefficients  $S_k$  and  $E_k$ , as determined from the empirical moments and across the parameters of log-normal distribution (see Eqs (7), (9) and (14), (15), is for illustration given for two examples: The empirical values of coefficient of skewness  $S_k$  2.24 and 2.42 correspond to the log-normal value 2.253.0 or 118.2. For the coefficient of excess  $E_k$  the corresponding empirical values were 4.98 and 6.14 and from the log-normal distribution both were -2.997. The difference in the momentum characteristics  $S_k$  and  $E_k$  according to the log-normal distribution in comparison with the empirical values is characteristic for the majority of experimental data<sup>1</sup> and confirms that the log-normal frequency function is not suitable for our purposes.

The distribution according to Schwarz and Bezemer (Eqs (2) or (6)) was not directly verified due to negative results with testing of regression dependence (3), the linearity of which determines suitability of this distribution for the given data. In Figs 2 to 4 logarithms of empirical cumulative volumetric fractions are plotted for the experiments of Katinger<sup>8</sup> (Figs 2 and 3) and for one series of our own data in Fig. 4. Dependences for other original data have an analogical character. In these Figs are further plotted the regression dependences according to Eq. (3). From given Figs

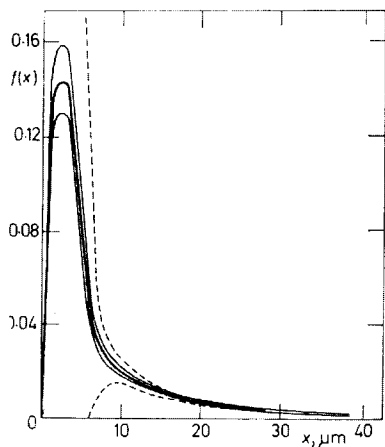


FIG. 1

Error of Frequency Function for Selected Experiment (Exp. 68b (ref.<sup>15,16</sup>))

—  $f(x)$ , ——— lines limiting the region  $f(x) \pm 0.1 \cdot f(x)$ , - - - lines of relative deviations according to Eq. (12).

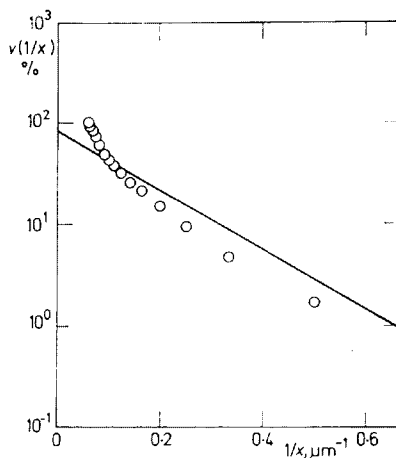


FIG. 2

Cumulative Volume Fractions According to Eq. (3)

○ Empirical values (Exp. K 1, Table I),  
— regression dependence.

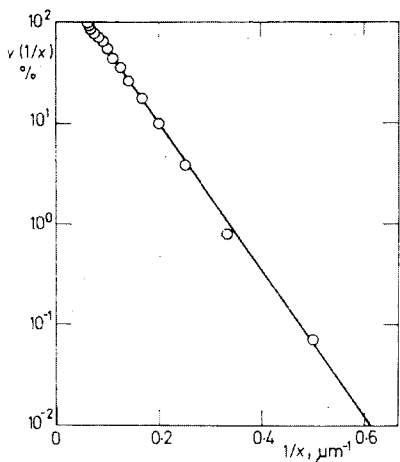


FIG. 3

Cumulative Volume Fractions According to Eq. (3)

○ Empirical values (Exp. K 3), — regression dependence.

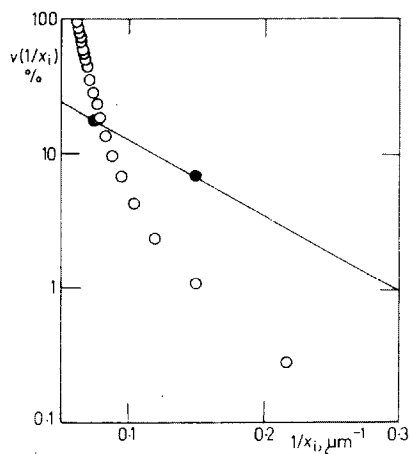


FIG. 4

Cumulative Volume Fractions According to Eq. (3)

○ Empirical values (Exp. 106 (ref.<sup>15,16</sup>))  
— regression dependence.

TABLE I  
Conditions of Experiments and Results of Calculations

Run No see ref <sup>15,16</sup>	$f^a, h$	$\phi^b$	Pearson's		Distribution parameters				Note			
			types of distributions		type X		type XII			(type III) <sup>c</sup>		
			main	alternative	$s$	$Y_0$	$M$	$B$		$N^d$		
			type	type	$\chi^2$	(G)	(P)	(A)				
32a	0.5	0.03	XII	X	161.2	11.96	61.3	0.668	5.14	—	766	time dependence, inoculum $X_0 = 0.5$ g/l
32b	3.0	0.03	XII	X	126.2	7.84	95.3	0.814	2.64	—	1 162	
32c	5.5	0.03	XII	X	171.8	7.88	98.5	0.815	2.65	—	1 218	
32c'	5.5	0.03	X	—	164.1	6.76	—	—	—	—	1 166	
32c''	5.5	0.03	X	—	136.6	6.68	—	—	—	—	1 043	
32d	8.0	0.03	X	—	176.5	7.76	—	—	—	—	1 249	
32d'	8.0	0.03	X	—	151.5	8.12	—	—	—	—	1 319	
32e	10.5	0.03	X	—	182.6	6.28	—	—	—	—	1 358	
32e'	10.5	0.03	X	—	159.0	5.78	—	—	—	—	1 410	
32f	23.5	0.03	XII	XII	278.9	7.99	100.7	0.722	3.20	—	965	
14a	1.5	0.03	XII	X	24.3	10.44	49.1	0.703	4.30	—	579	time dependence, inoculum $X_0 = 0.8$ g/l
14b	4.0	0.03	XII	III	91.1	—	120.6	0.787	2.47	—	1 189	
14b'	4.0	0.03	XII	X	76.7	6.12	(123.9)	(0.261)	(-0.181)	(3.14)	—	
14c	6.5	0.03	XII	III	71.8	—	142.6	0.832	1.96	—	1 460	
14c'	6.5	0.03	XII	II	49.4	—	180.7	0.821	1.67	—	1 453	
14c''	6.5	0.03	XII	II	49.4	—	(203.3)	(0.318)	(-0.354)	(2.03)	—	
14c'''	6.5	0.03	XII	III	97.0	—	157.1	0.831	1.75	—	1 419	
14c''''	6.5	0.03	XII	III	97.0	—	(182.0)	(0.283)	(-0.401)	(2.11)	—	
14c'''''	6.5	0.03	XII	III	97.0	—	178.4	0.802	1.68	—	1 297	
14c''''''	6.5	0.03	XII	III	97.0	—	(190.4)	(0.353)	(-0.259)	—	—	

14d	9.5	0.03	X	63.2	XII	78.3	4.96	165.6	0.817	1.67	—	1.306
14d'	9.5	0.03	X	85.5	XII	69.5	4.68	208.1	0.811	1.65	—	1.520
14d''	9.5	0.03	X	34.5	III	48.1	4.12	(230.3)	(0.442)	(-0.158)	(1.89)	1.318
14d'''	9.5	0.03	X	52.3	XII	68.3	4.32	184.3	0.828	1.42	—	1.318
14e	12.5	0.03	X	90.6	XII	127.0	3.96	240.4	0.802	1.38	—	1.435
14e'	12.5	0.03	X	63.6	XII	86.7	3.92	199.5	0.810	1.34	—	1.214
13a	0.75	0.03	X	134.3	III	132.3	8.46	(117.5)	(0.238)	(0.017)	(4.274)	1.349
13b	3.5	0.03	X	105.3	III	181.2	6.51	(220.7)	(0.281)	(-0.156)	(3.00)	1.988
13c	6.75	0.03	X	49.7	—	—	4.61	—	—	—	—	1.576
13c'	6.75	0.03	X	49.5	XII	84.5	4.36	267.9	0.777	1.60	—	1.626
13c''	6.75	0.03	X	88.4	XII	90.4	4.25	226.2	0.835	1.45	—	1.729
13d	9.5	0.03	X	49.9	XII	128.4	3.28	256.9	0.821	1.09	—	1.361
13d'	9.5	0.03	X	81.6	XII	100.0	4.30	251.0	0.814	1.45	—	1.694
13d''	12.5	0.03	X	79.6	XII	77.5	5.00	196.7	0.804	1.74	—	1.493
13e'	12.5	0.03	X	118.7	XII	95.7	5.24	164.8	0.815	1.76	—	1.352
13e''	12.5	0.03	X	65.5	XII	67.4	5.04	161.6	0.819	1.68	—	1.302
68a	4.5	0.015	X	109.3	—	—	6.18	151.1	0.828	2.01	—	1.538
68b	4.5	0.015	XII	75.2	—	—	—	116.9	0.812	2.48	—	1.329
106	5.0	0.03	XII	46.0	III	72.0	—	182.6	0.766	2.76	—	1.606
102	6.0	0.05	XII	282.8	X	292.8	7.44	(31.1)	(0.261)	(-0.061)	(3.60)	2.217
62a	6.0	0.10	XII	52.0	—	—	—	197.5	0.810	2.47	—	1.704
62b	6.0	0.10	XII	41.0	—	—	—	117.2	0.790	3.61	—	1.548
121	7.0	0.10	XII	48.0	—	—	—	109.5	0.762	4.03	—	1.374
47a	6.0	0.10	XII	180.8	X	215.9	5.97	83.9	0.818	3.44	—	962
47b	6.0	0.10	XII	133.1	—	—	—	94.4	0.838	1.89	—	1.167
48	5.0	0.108	X	164.5	XII	211.7	6.90	106.1	0.842	1.97	—	1.041
								101.0	0.801	2.39	—	

time dependence,  
inoculum  
 $X_0 = 1.5 \text{ g/l}$

effect of volume  
fraction of  
dispersed phase

fermentor with  
volume  $1 \text{ m}^3$

\*

TABLE I  
(Continued)

Run No	$t^a$ , h	$\phi^b$	Pearson's		Distribution parameters				Note		
			Types of distributions		type X	type XII		(type III) <sup>c</sup>			
			main	alternative		$s$	$Y_0$			$M$	$B$
type	$\chi^2$	type	$\chi^2$		(G)	(P)	(A)	$N^d$			
W1	—	—	III	52.0	—	(172.8)	(0.549)	(4.72)	(10.42)	—	W1—600 r.p.m. <sup>9</sup>
W2	—	—	III	54.0	—	(193.8)	(0.739)	(3.79)	(6.48)	—	W2—800 r.p.m. <sup>9</sup>
W3	—	—	III	54.0	—	(187.6)	(0.884)	(4.09)	(5.76)	—	W3—1000 r.p.m. <sup>9</sup>
K1	—	—	XII	24.0	—	224.8	0.966	0.164	—	—	K1—mechanically agitated fermentor <sup>7</sup>
K2	—	—	XII	63.0	X	67.0	0.772	1.98	—	—	K2—mechanically agitated fermentor <sup>7</sup>
K3	—	—	III	18.0	—	(212.6)	(0.637)	(2.19)	(5.00)	—	K3—mechanically agitated fermentor <sup>7</sup>

<sup>a</sup>  $t$  is the time from the beginning of fermentation. <sup>b</sup>  $\phi$  is the volume fraction of the dispersed phase. <sup>c</sup> Values of parameters for type III are given in brackets. <sup>d</sup>  $N$  is the size of the sample.

2 to 4 is obvious that the regression dependence (3) for fermentors intensively agitated by mechanical agitators does not fit the empirical values and distributions according to Schwarz and Bezemer thus are not suitable for the cases considered by us. Of all the studied systems it is suitable only for the bubble-type fermentor according to Katinger<sup>5</sup>.

## EXPERIMENTAL

The laboratory fermentor is a cylindrical vessel with radial baffles having a volume 1.5 l, intensively agitated (speed of rotation of the impeller  $1000 \text{ min}^{-1}$ ) by a non-standard turbine mixer situated in a cylindrical drought tube. Description of the mixer (modified mixer according to Waldhof) together with the detailed description of the apparatus and conditions of the fermentation experiments and properties of the used substances are given in the earlier publications of this series<sup>15,16</sup>. Numbering of experimental runs in all these publications is identical. Several experiments were performed with a pilot-plant fermentor of 1000 l volume. This fermentor was mixed by several mixers with drought tubes<sup>17</sup>. In both experimental units the samples were taken from the region of the mixer and in the pilot-plant fermentor also from the circulation part of the vessel.

The complete description of the experimental method for determination of the drop size distribution by stabilization of samples in gelatine is given in the preceding paper of this series<sup>18</sup>. The fermentation experiments were performed batchwise. In three experiments has been studied the time dependence of distribution for different sizes of inoculus of the yeast culture. Further the effect of fraction of the hydrocarbon phase in the dispersion was studied. The conditions of the experiments are given in Table I together with the calculation results.

## FREQUENCY FUNCTIONS ACCORDING TO PEARSON

Because of the negative results with the until now published relations for the frequency function for drop sizes in emulsion and due to great complexity of the given system, an attempt has been made to find a new empirical relation. The system of frequency functions<sup>19</sup> according to Pearson was chosen because of its universal application. This system includes 13 types of frequency functions whose parameters can be determined through the first four moments about origin of the system. The details of calculation are not presented here, they can be found *e.g.* in the monography by Elderton and Johnson<sup>19</sup> and for their realization the program published by Chisman<sup>20</sup> has been modified. Preliminary results of tests of all types on about 10 experiments made by us have demonstrated that types II, IV and VIII are not suitable for mathematical reasons. Further on, the frequency functions of types I, V, VII, IX, XI and the normal distribution have completely unsuitable dependences with respect to the empirical frequency function. Therefore the selection of types of Pearson's functions has been narrowed to the types III, X, and XII.

The number of drops fitting the frequency function of type III can be determined from the relation

$$n_0 = Y_0(1 + x/A)^P \exp(-Gx). \quad (16)$$



Parameters of distribution  $Y_0$ ,  $A$ ,  $P$ , and  $G$  can be determined from following relations

$$Y_0 = N \cdot G(P + 1)^P / [\exp(P + 1) \cdot \Gamma(P + 1)], \quad (17)$$

$$A = (P + 1)/G, \quad (18)$$

$$P = 4B_1 - 1, \quad (19)$$

$$G = 2m_2/m_3, \quad (20)$$

$$B_1 = t_3^2/t_2^3. \quad (21)$$

In Eqs (17) to (21)  $m_2$  and  $m_3$  are the central moments of the second and third order,  $N$  is the size of sample,  $B_1$  is the coefficient asymmetry due to Pearson,  $t_2$  and  $t_3$  are the transformed central moments for the grouped empirical frequencies  $\{x_i, n_{ie}; \Delta x\}$  which for the case of equidistant classes of drop sizes ( $\Delta x = \text{const}$ ) can be determined from the relation

$$t_j = m_j/(\Delta x)^j. \quad (22)$$

Frequency for the type X are defined by the relation (negative exponential curve)

$$n_0 = N \{ \exp [ -(x/s) - 1 ] \} / s. \quad (23)$$

This function has a single parameter – the standard deviation  $s$ .

The frequencies according to type XII have the form

$$n_0 = Y_0 (s\beta^+ - x)^M (s\beta^- + x)^{-M}, \quad (24)$$

as long as the third central moment is positive ( $m_3 > 0$ ) and

$$n_0 = Y_0 (s\beta^+ + x)^M (s\beta^- - x)^{-M}, \quad (25)$$

as long as  $m_3 < 0$ . The empirical parameters in Eqs (24) and (25) can be calculated from relations

$$\beta^+ = (3 + B_1)^{1/2} + B_1^{1/2}, \quad (26)$$

$$\beta^- = (3 + B_1)^{1/2} - B_1^{1/2}, \quad (27)$$

$$M = [B_1/(3 + B_1)]^{1/2}, \quad (28)$$

$$Y_0 = N/[B \cdot \Gamma(1 + M) \Gamma(1 - M)], \quad (29)$$

$$B = 2[m_2(3 + B_1)]^{1/2}, \quad (30)$$

in which the  $\Gamma(a)$  is the complete gamma function value of argument  $a$ . Frequencies calculated from relations (16), (23), (24) or (25) were corrected by relation

$$n_i = n_0 \cdot N/N_0, \quad (31)$$

where  $N$  and  $N_0$  are sums of empirical and theoretical frequencies respectively. By this arrangement the normalization of calculated frequencies is obtained *i.e.*  $\sum_i n_{ic} = \sum_i n_{it}$ .

For the graphical comparison of results the empirical and theoretical frequency functions were calculated

$$f(x_i) = n_i/\Delta x \sum_i n_i, \quad (32)$$

where  $\Delta x$  is the width of the size interval of empirical distribution of drop frequencies (grouped distribution). The agreement of empirical and theoretical distributions has been considered according to the uncorrected value  $\chi^2$  of the criterion of goodness of fit which is defined by relation

$$\chi^2 = \sum_i [(n_{it} - n_{ic})^2/n_{ic}]. \quad (33)$$

Neither grouping of frequencies in calculation (33) nor other goodness tests of fit have been used.

## RESULTS AND DISCUSSION

In Table I is presented the summary of results of distributions according to Pearson both for our own data as well as for data by Katinger<sup>7,8</sup> and by Wang-Ochoa<sup>9</sup>. As the main is always considered the type of distribution with the minimum value of  $\chi^2$  criterion. As long as for one of the considered types the value of  $\chi^2$  is smaller than the twice of  $\chi^2$  value for the main type, the given distribution is considered as an alternative type. In the other part of the Table are given parameters of the considered types. Mostly the types X and XII\* are concerned. The values of parameters for the type III are denoted by an asterisk. In Table I is also given the size of samples from which the parameters were calculated.

\* In all considered cases hold  $m_3 > 0$  so that the type XII was calculated from the relation (24).

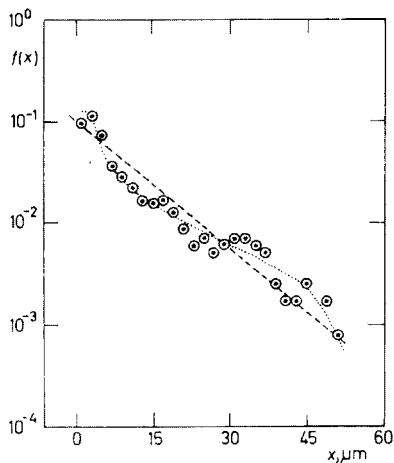


FIG. 5

Distribution According to Pearson of the Types X and XII (exp. 14a (ref.<sup>15,16</sup>))

○ Empirical frequency function, ---- Pearson's type X distribution, ..... Pearson's type XII distribution.

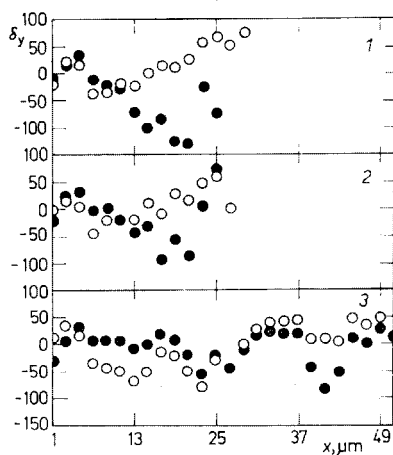


FIG. 6

Relative Deviations ( $\delta_y$ , %) of Frequency Functions of the Types X and XII (exp. 14a (ref.<sup>15,16</sup>))

○ Type X, ● type XII; 1  $t = 12.5$  h, 2  $t = 9.5$  h, 3  $t = 1.5$  h.

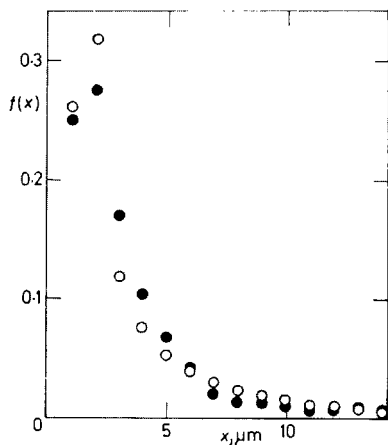


FIG. 7

Pearson's Type XII Distribution

● Empirical frequency function ( $K_2$ , Table I), ○ Pearson's type XII frequency function.

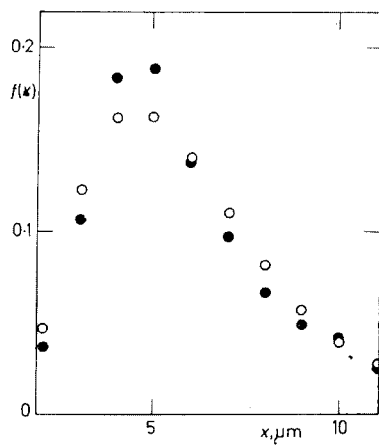


FIG. 8

Pearson's Type III Distribution

● Empirical frequency function ( $K_3$ , Table I), ○ Pearson's type III frequency function.

*The time dependence.* From Table I is obvious that for the sets of drops formed at the beginning of fermentation for small values of inocula ( $X_0 = 0.5$  and  $0.8$  g/l), the type XII seems to be more suitable than the type X which is suitable for systems at the end of fermentation and for larger values of inocula. This trend is in agreement with the change of the coefficient of excess  $E_k$  (see<sup>1</sup>). The type XII is suitable for systems with smaller peakedness. The graphical comparison of distributions of types XII and X with the empirical frequency function for the system from the beginning of fermentation is in semi-log coordinates given in Fig. 5. In these coordinates the type X is linearised and thus it is stressed that this type is not suitable for the given conditions. For illustration of selection between the types X and XII and for graphical localisation of deviations for one selected experiment are in Fig. 6 also given the relative deviations between the empirical and theoretical frequency functions (distributions according to Pearson of types X and XII)  $\delta_y$  for various times from the beginning of fermentation. If we neglect the deviations in the region of large particles (above  $20 \mu\text{m}$ ) which, due to the small interval frequencies are not statistically significant, it can be said that the deviations dependence on the size of drops are for both types analogous and differs with the type only in magnitude.

*Volume fraction of hydrocarbon phase.* The volume fraction  $\Phi$  has been varied from 1.5 to 10 vol. %. The time in which the samples were taken was about the first third of the total time of fermentation<sup>1</sup>. We came to the conclusion that at higher concentrations of the hydrocarbon phase the suitability of the type XII was prevailing.

*Data of other authors.* Katinger<sup>7,8</sup> has studied emulsification of the gas oil (volume fraction 10%). For the fermentor with a mechanical mixer the Pearson's distribution of the type XII is suitable (Fig. 7) while for a less intensively agitated bubble-type

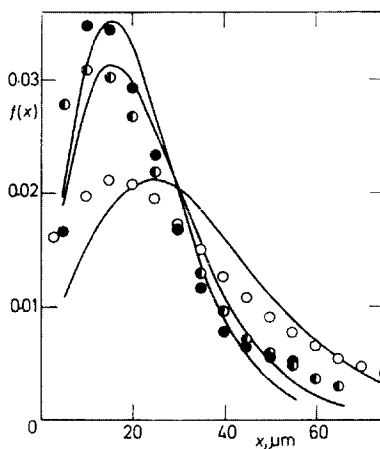


FIG. 9

Pearson's Type III Distribution, Data No. W 1 to W 3

○ Empirical values (W 1, Table I), ◐ empirical values (W 2), ● empirical values (W 3), — theoretical frequency function.

fermentor is more suitable the type III (Fig. 8). Wang and Ochoa<sup>9</sup> are presenting distributions of n-hexadecane in the media with yeasts obtained at various mixing intensities with a standard turbine mixer. These distributions of drop sizes obtained by sedimentation were before evaluation normalized as they have not fulfilled the condition for the frequency function  $\int_x f_c(x) dx = 1$ . Distribution according to these authors has a considerably lesser peakedness and can be described regardless of the mixing intensity by the Pearson's type III (Fig. 9).

Finally, it can be concluded that the system of frequency functions according to Pearson has been found suitable for distributions of drop size at fermentation of hydrocarbons. By this way quite different shapes of frequency functions can be described which are characterized by a different skewness and asymmetry. Some new information were obtained concerning the usability of individual types under certain fermentation conditions. Correlation of distribution parameters with the conditions will require additional experiments.

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